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Power Quality Improvement in DTC of Induction Motor Drive Using VSC Based STATCOM

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ABSTRACT: A The Power Quality (PQ) in distribution system is affected during its starting whn it draws large current. Voltage Sag is one of the Power Quality problem created by the induction motor. When it is connected to a source, there is a dip in the voltage which could be critical for the entire system. The power electronics based fact devices called static synchronous compensator (STATCOM) used in this paper to improve power quality during starting of induction motor with dtc scheme . The result will be analysed by comparing the THD of the source side with and without statcom. Among all control methods for induction motor drives, Direct Torque Control (DTC) seems to be particularly interesting being independent of machine rotor parameters and requiring no speed or position sensors.This paper is aimed to analyze DTC of induction motor with statcom for power quality improvement.

KEYWORDS: Direct torque control (DTC), induction motor, Power Quality, Voltage Source Converter (VSC), Statcom, THD

I. INTRODUCTION

The DTC based induction motor drive (IMD) uses a single-phase or three-phase uncontrolled ac-dc converter (for rectification of ac mains voltage), an energy storage element (capacitor filter for smoothening the dc link voltage), and a three-phase voltage source inverter (VSI) for feeding a three-phase squirrel cage induction motor. Such type of utility interface suffers from problems related to power quality such as poor power factor, injection of current harmonics into the ac mains, variation in dc link voltage with fluctuations in the voltage of input ac supply, equipment overheating due to harmonic current absorption, voltage distortion at the point of common coupling (PCC) due to the voltage drop caused by harmonics currents flowing through system impedance and decreased rectifier efficiency. These power quality problemscan cause malfunction of sensitive electronic equipments, interference in telephone and communication lines due to highfrequency switching, failure of switching capacitors and other power equipment and loss of data.

Early STATCOM generally used the zigzag transformer in the main circuit topology as voltage source inverter. However, the zigzag transformer has some difficulties, which is hard to overcome in terms of cost, transformer loss as well as the control. When the inverter is used as the main circuit topology, STATCOM has a little floor space, easy to split-phase control, high reliability, and easy expansion of capacity, etc. In addition, because it has no use for the zigzag transformer, it makes the existing STATCOM free of the most serious problems such as device over-voltage caused by the magnetic saturation and nonlinearity in the transformer excitation circuit .So the inverter structure for large capacity STATCOM is concerned by a large number of engineering designers more and more.

II. DTC BASED INDUCTION MOTOR DRIVE

In principle the DTC method selects one of the six nonzero and two zero voltage vectors of the inverter on the basis of the instantaneous errors in torque and stator flux magnitude.

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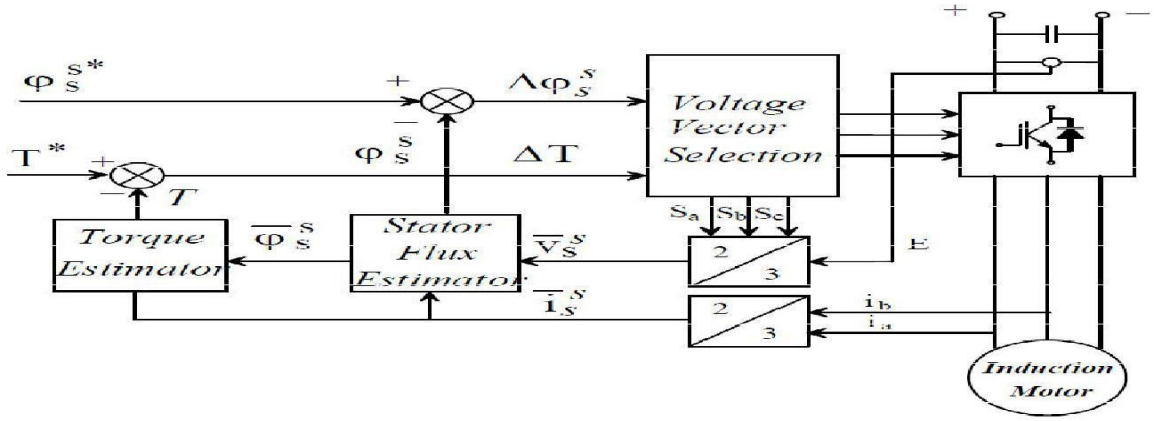
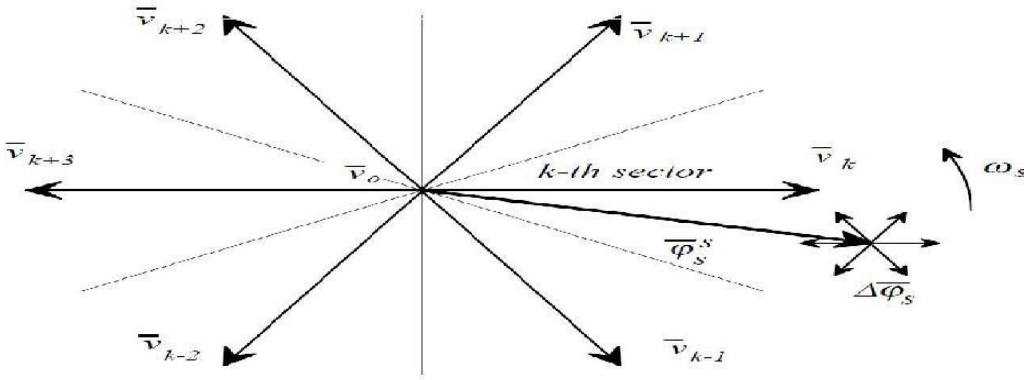


Assuming the voltage drop Rsiss small, the stator flux is driven in the direction of the stator voltage v

ss $\Delta\bar{\varphi}_s^s \cong \bar{v}_s^s \, \Delta T$ where T is the sampling period



$v_k \Rightarrow$ radial positive voltage vector
$v_{k+1} \Rightarrow$ forward positive "
$v_{k+2} \Rightarrow$ forward negative "
$v_{k+3} \Rightarrow$ radial negative "
$v_{k-1} \Rightarrow$ backward positive "
$v_{k-2} \Rightarrow$ backward negative "
$v_0 \; e \; v_7 \Rightarrow$ zero "

The flux variation is proportional to E, T and has the same direction of the voltage vector applied

ROTOR FLUX AND TORQUE VARIATION

From the general equations written in the rotor reference frame, we can derive

$$\varphi_r^r = \frac{L_m}{L_s} \frac{1}{1 + s\sigma\tau_r} \varphi_s^r \qquad \text{with} \qquad \sigma = 1 - \frac{L_m^2}{L_s L_r}$$

This equation shows the nature of rotor flux dynamic response for changes in stator flux

$$T = \frac{3}{2} p \frac{L_m}{\sigma L_s L_r} \bar{\varphi}_s^r \cdot j\,\bar{\varphi}_r^r = \frac{3}{2} p \frac{L_m}{\sigma L_s L_r} \varphi_s \, \varphi_r \sin \vartheta_{sr}$$

Any stator flux vector variation determines a torque variation on the basis of two contributions

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I) The variation of the stator flux magnitude

II) The variation of the stator flux phase angle with respect to rotor flux

Any command which causes the flux angle to change will determine a quick torque variation.

III. WORKING OF STATCOM

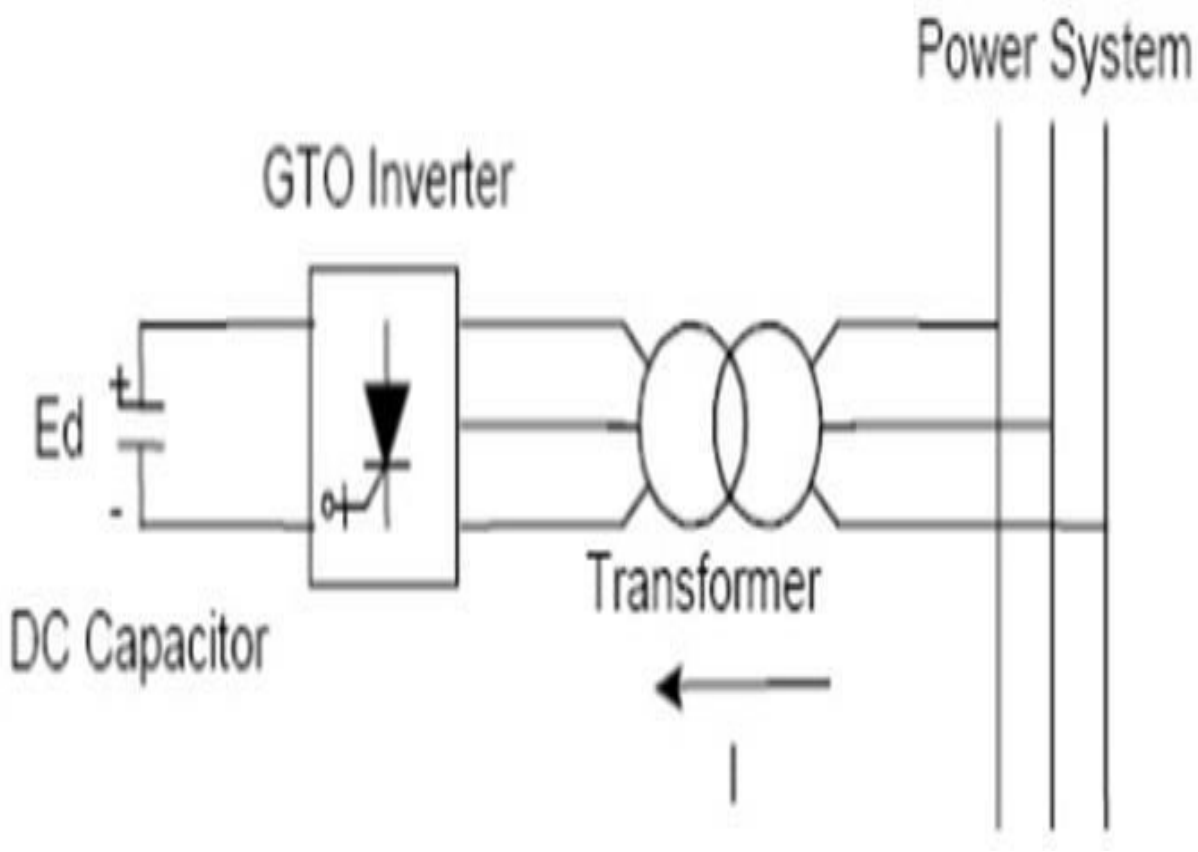

Fig:-STATCOM

In the case of two AC sources, which have the same frequency and are connected through a series reactance, the power flows will be:

Active or Real Power flows from the leading source to the lagging source.

Reactive Power flows from the higher to the lower voltage magnitude source.

Consequently, the phase angle difference between the sources decides the active power flow, while the voltage magnitude difference between the sources determines the reactive power flow. Based on this principle, a STATCOM can be used to regulate the reactive power flow by changing the output voltage of the voltage-source converter with respect to the system voltage.

Modes of Operation

The STATCOM can be operated in two different modes:

A. Voltage Regulation

The static synchronous compensator regulates voltage at its connection point by controlling the amount of reactive power that is absorbed from or injected into the power system through a voltage-source converter.

In steady-state operation, the voltage V2 generated by the VSC through the DC capacitor is in phase with the system voltage V1 (δ=0), so that only reactive power (Q) is flowing (P=0).

1. When system voltage is high, the STATCOM will absorb reactive power (inductive behavior)
2. When system voltage is low, the STATCOM will generate and inject reactive power into the system (capacitive). Subsequently, the amount of reactive power flow is given by the equation:

Q = [V1(V1-V2)] /

X B. Var Control

In this mode, the STATCOM reactive power output is kept constant independent of other system parameter.

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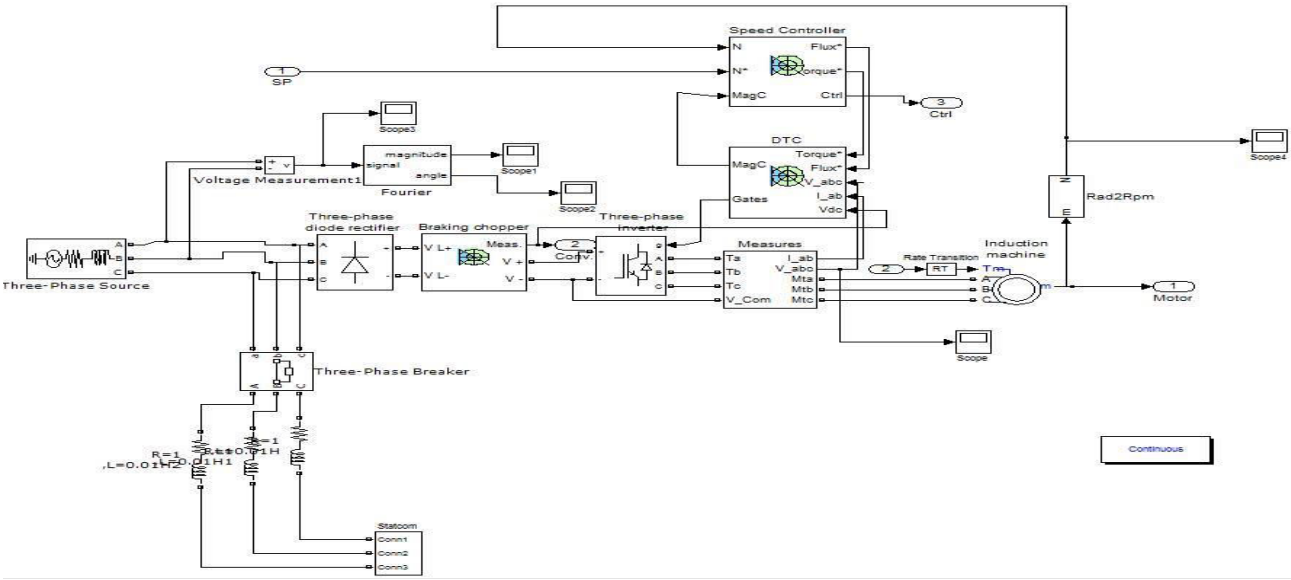
IV. SIMULATION

With the help of the MATLAB Simulink model of three phase induction motor and STATCOM is easily established .The following figure (shows the various parts of the motor model with

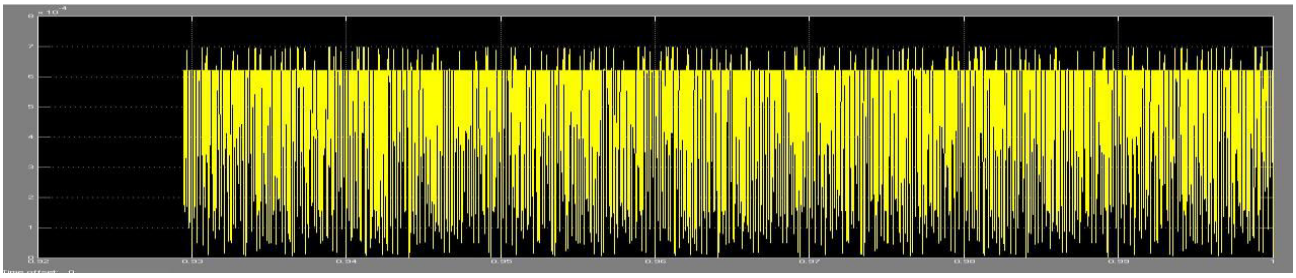


The speed controller is based on a PI regulator, shown below. The output of this regulator is a torque set point applied to the DTC controller block.The Torque & Flux calculator block is used to estimate the motor flux αβ components and the electromagnetic torque. This calculator is based on motor equation synthesis.The αβ vector block is used to find the sector of the αβ plane in which the flux vector lies. The αβ plane is divided into six different sectors spaced by 60 degrees.The Flux & Torque Hysteresis blocks contain a two-level hysteresis comparator for flux control and a three level hysteresis comparator for the torque control. The description of the hysteresis comparators is available below.The Switching table block contains two lookup tables that select a specific voltage vector in accordance with the output of the Flux & Torque Hysteresis comparators. This block also produces the initial flux in the machine.The Switching control block is used to limit the inverter commutation frequency to a maximum value specifiedby the user.

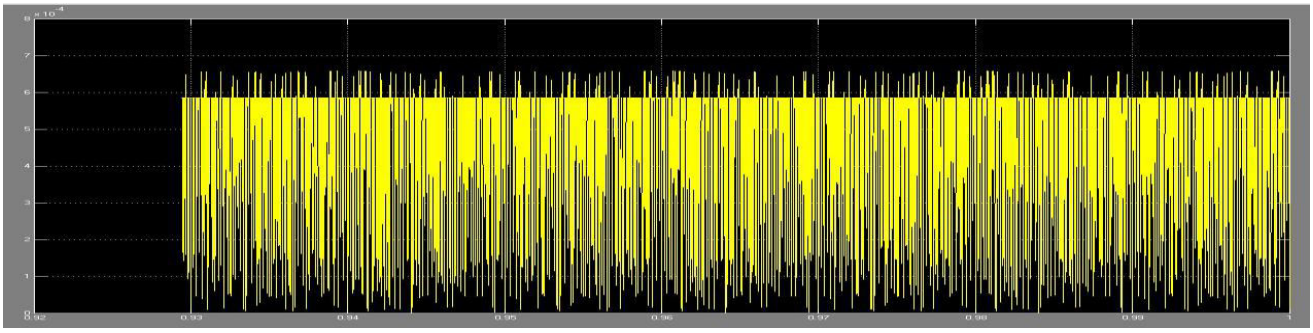
V. RESULTS AND DISCUSSIONS

Performance of the DTC based IMD is studied for both the configurations namely, with and withoutSTATCOM at the front end. Waveforms consist of Fourier and FFT of source phase voltage (vas)rotor speed (Nr), electromagnetic torque (Te) for the rating of 5 HP, 460V, 60Hz, 1750rpm The ac mains voltage waveform and its harmonic spectra at load is shown in which show that THD at no load. From these results it can be concluded that it is necessary to use improved power quality converters at front end of the DTC based IMD. As the next step, a STATCOM is employed in the waveforms of a DTC based IMD for load conditions fed from a STATCOM at the front end are shown in The ac mains current and its harmonic spectra for load.Fourier response with response show ripple within .09% and .07% with stacom. It can be noted that the THD of ac mains voltage at load is 0.01%. A significant improvement as compared to the case without statcom where THD is 24.9%.Fourier response with and without statcom are shown

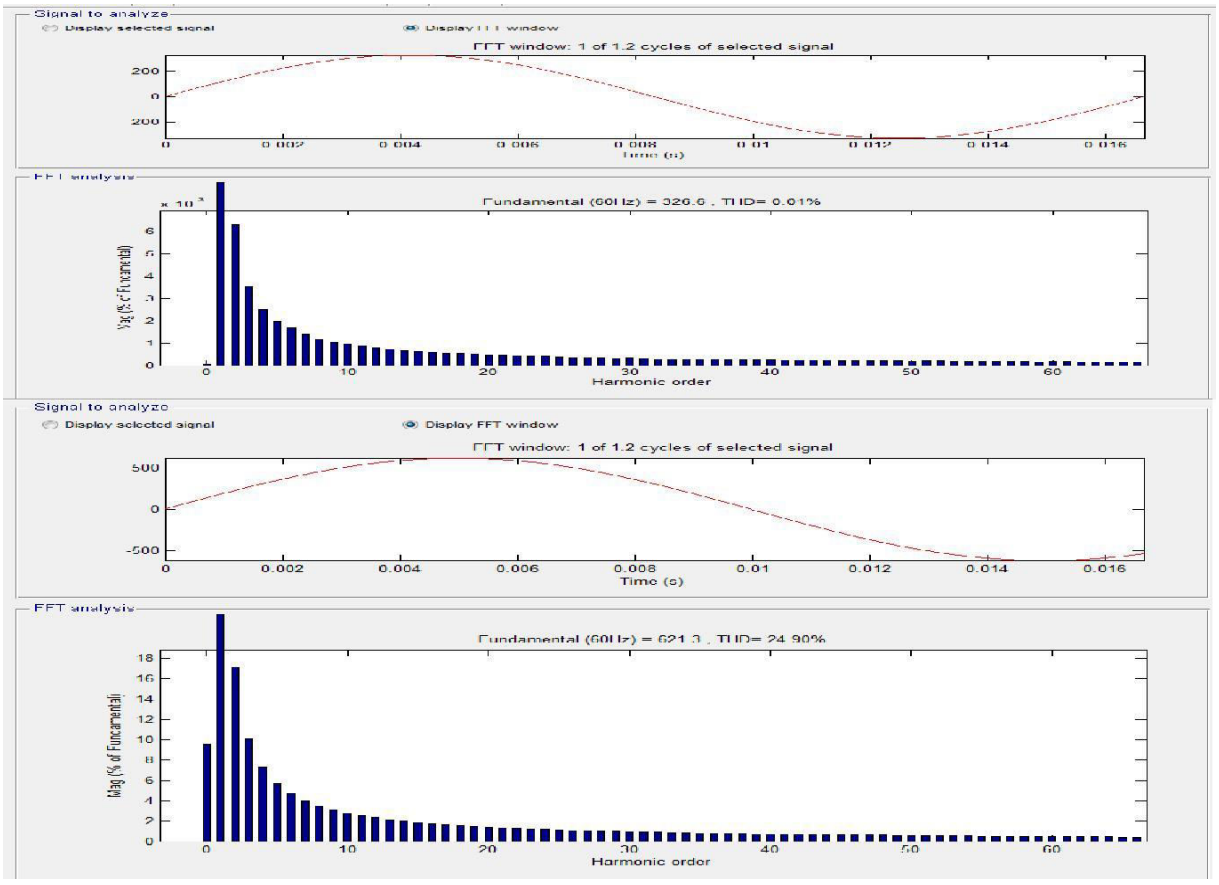
A. Without statcom



B.Withstatcom



C.FFT (WITHOUT STACOM) THD=24.9%



D.FFT(WITH STATCOM) THD=0.01%

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